

Investigating the relationship between CAD model complexity and performance trade-offs for fusion neutronics

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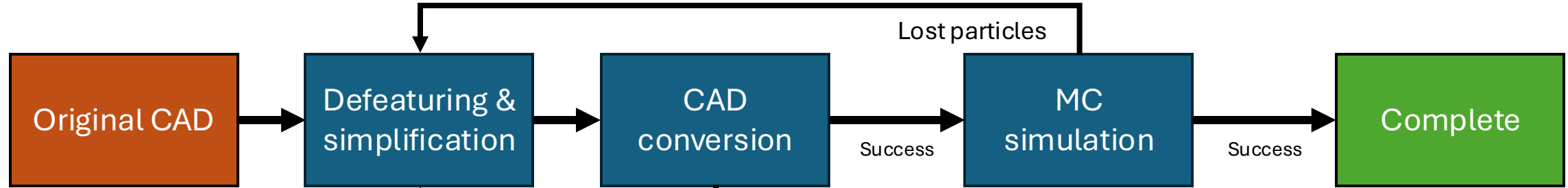
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2025 Fusion Neutronics Meeting: ITER and Beyond

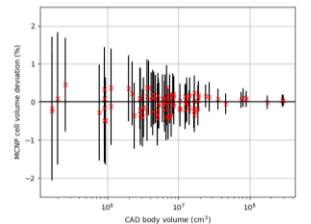
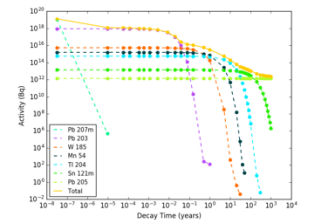
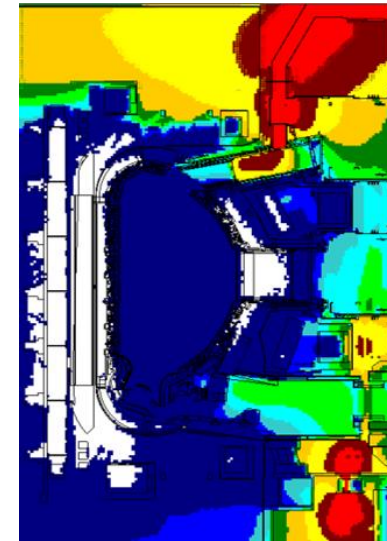
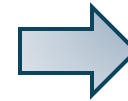
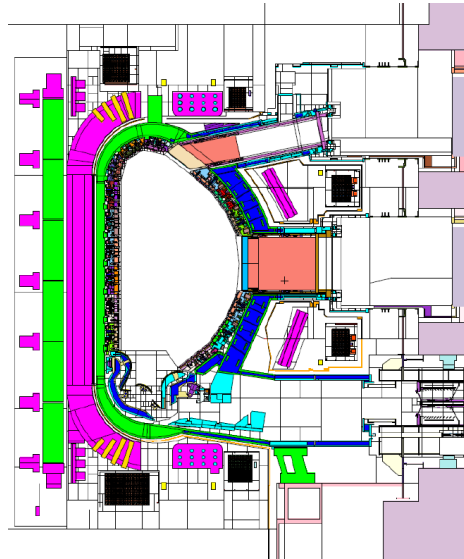
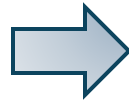
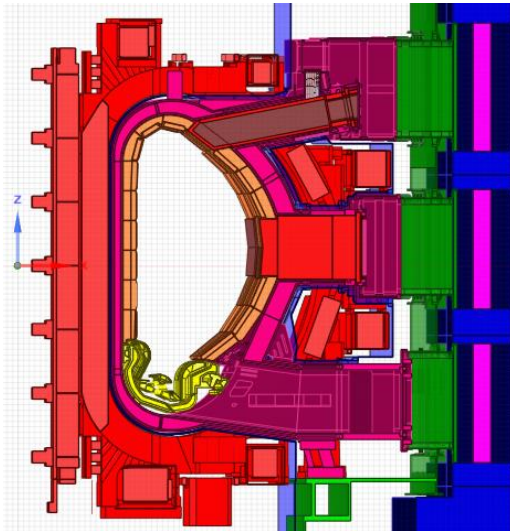
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April 2025

A typical neutronics workflow

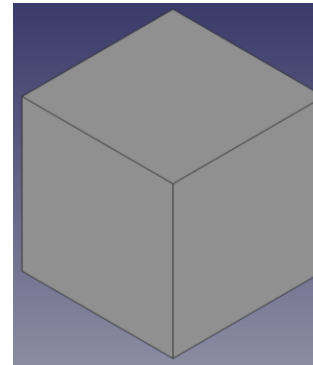


GeoUNED, McCAD,
SuperMC, Coreform Cubit



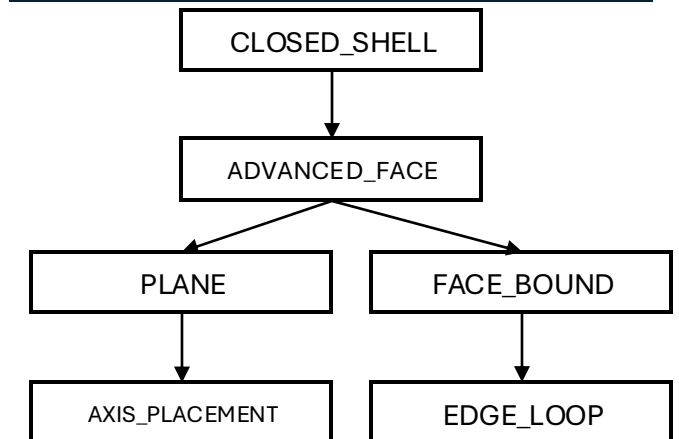
- Real-world models need to be defeatured prior to running a simulation
 - Defeaturing is manual and often error-prone
- We want to automate defeaturing, but that requires understanding geometry complexity
 - We need quantifiable metrics to decide *when* to defeature and *how much*
- To do this..
 - We implement the complexity measurement introduced in ^[1], comparing quantifiable metrics with so-called expert grading
 - Includes graph- and geometry-based metrics, applying them to STEP files

STEP File



```
. . .  
#79 = EDGE_CURVE('',#72,#80,#82,.T.);  
#80 = VERTEX_POINT('',#81);  
#81 = CARTESIAN_POINT('',(10.,10.,10.));  
#82 = LINE('',#83,#84);  
#83 = CARTESIAN_POINT('',(10.,10.,0.));  
#84 = VECTOR('',#85,1.);  
#85 = DIRECTION('',(0.,0.,1.));  
#86 = ORIENTED_EDGE('',*,*,#87,.F.);  
#87 = EDGE_CURVE('',#64,#80,#88,.T.);  
#88 = LINE('',#89,#90);  
#89 = CARTESIAN_POINT('',(10.,0.,10.));  
. . .
```

Graph representation

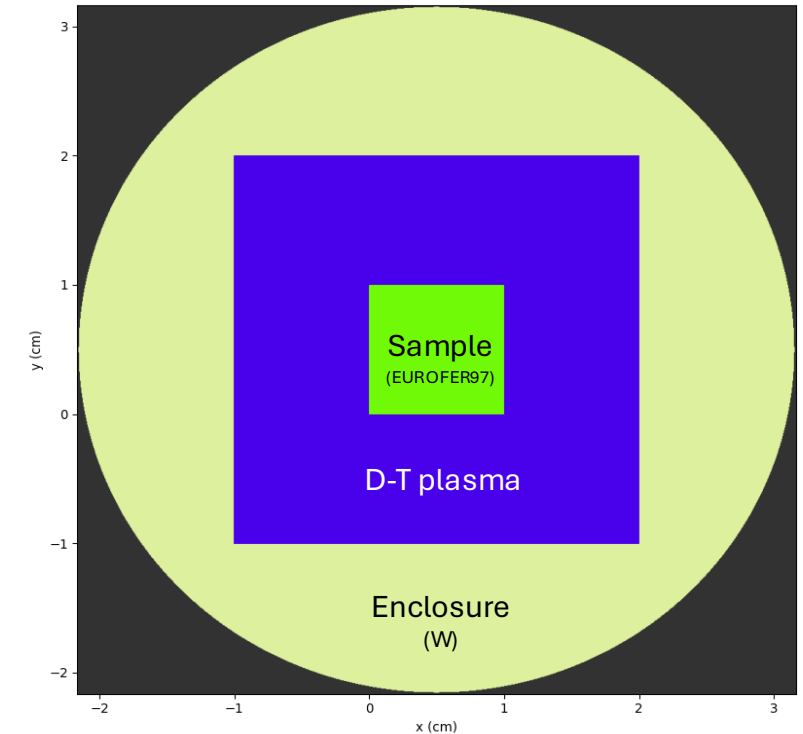


Methodology: quantifying model complexity

Metric name	Description	Spearman (ρ) (to practitioner grading)
Cyclomatic complexity	No. of independent paths through the graph	0.804
Kolmogorov complexity	String length when the graph is encoded as a binary string	0.801
Graph entropy	Description of graph uncertainty	0.799
Graph size	No. of nodes in the graph	0.792
Number of faces	Total number of individual faces in model	0.762
Graph dependencies	No. of edges in the graph	0.755
Number of vertices	Total number of individual vertices in model	0.713
Cube ratio	$1 - a_{\text{Cube}} / \text{Surface}$, a_{Cube} is area of a cube with the same volume as the model	0.428
Sphere ratio	$1 - a_{\text{Sphere}} / \text{Surface}$, a_{Sphere} is area of a sphere with the same volume as the model	0.428
Volume ratio	$1 - \text{Volume} / b_{\text{BoxVol}}$, b_{BoxVol} is volume of the bounding box of the model	0.414
Volume/area ratio	Ratio of surface area/object volume	-0.06

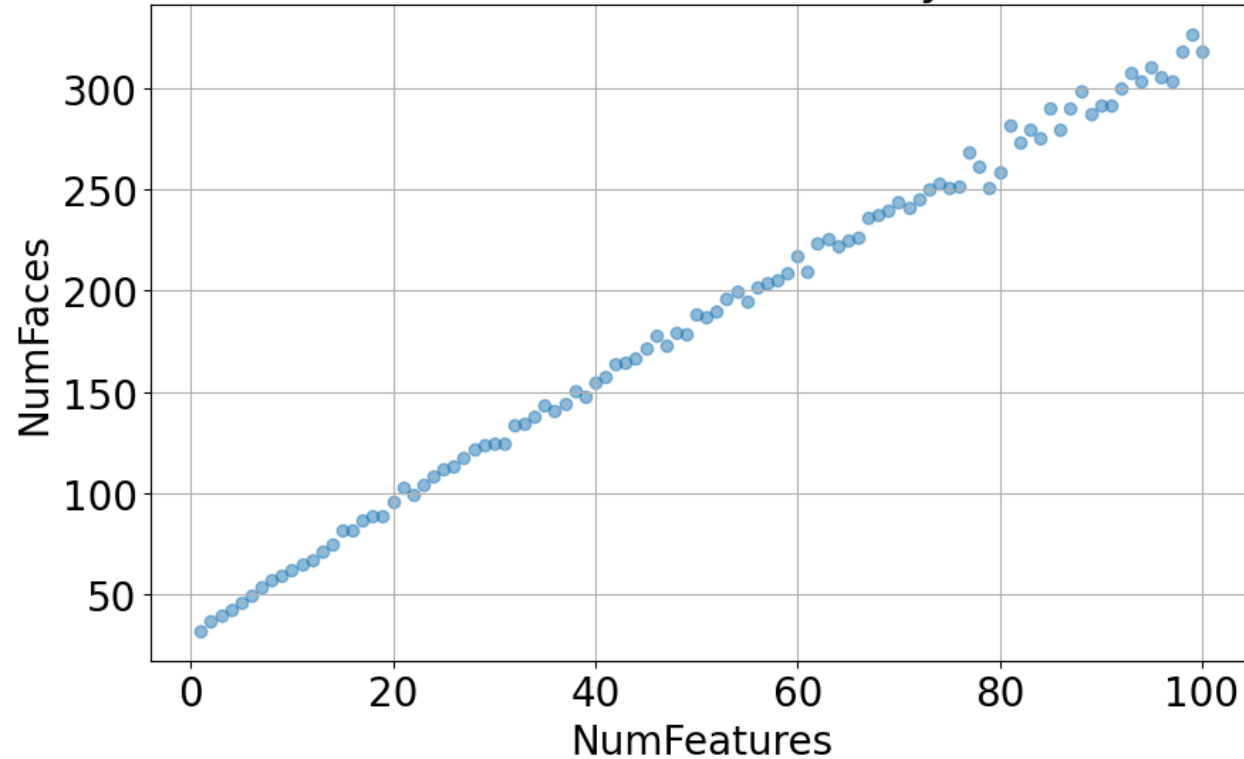
Methodology: simulation of a toy case

- Case: A 'box' of plasma with the sample geometry at centre
- Input:
 - Geometry from the MFCAD++ dataset ^[2], converted to CSG using GEOUNED ^[3]
 - 2 sets: one with protrusions and another with holes
- Simulation configurations
 - Source: Isotropic IndependentSource, located at (0,0,0)
 - Energy: Muir distribution @14.1MeV mean, $M_{\text{rat}}=5\text{AMU}$, $k_t=20000\text{eV}$
 - Materials:
 - Enclosure: W (100%),
 - Sample: EUROFER97 (composition as per ^[4])
 - Environment:
 - ARCHER2, standard partition, 16 cores per task
- Measured simulation outcome:
 - Tallies:
 - Flux: VITAMIN-J-175 energy group
 - Runtime
 - Measured as per OpenMC timing variables

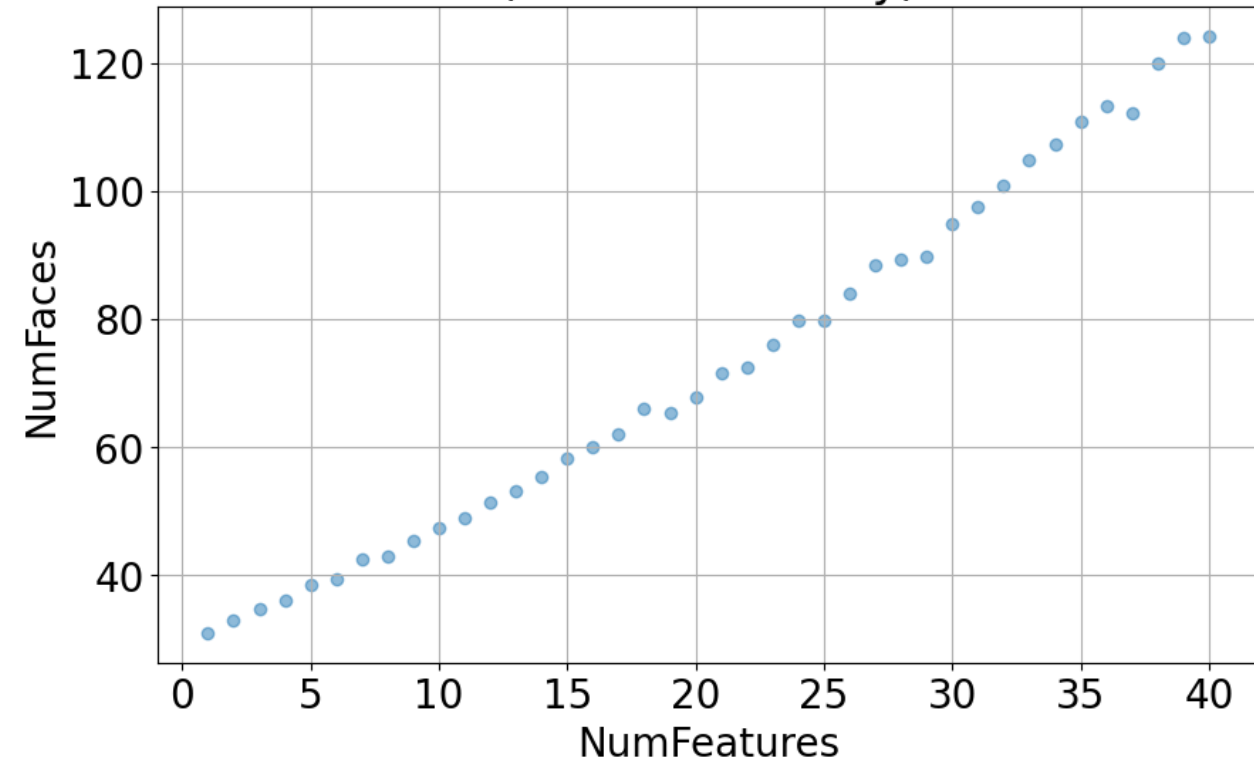


Results: starting simple

NumFeatures vs NumFaces
(Protrusion Geometry)



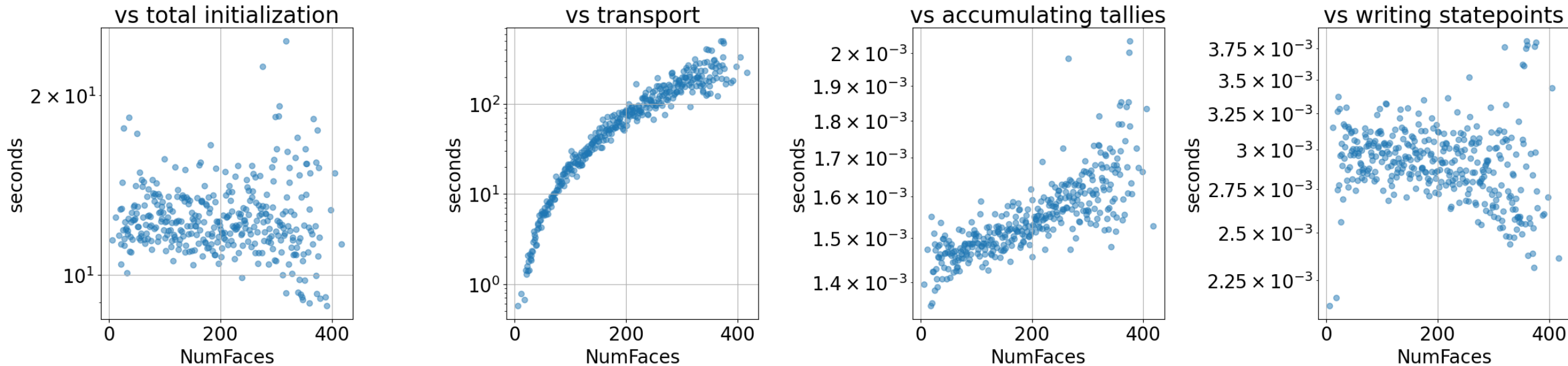
NumFeatures vs NumFaces
(Holes Geometry)



More features -> more faces (easy enough to understand!)

Results: runtime (protrusions)

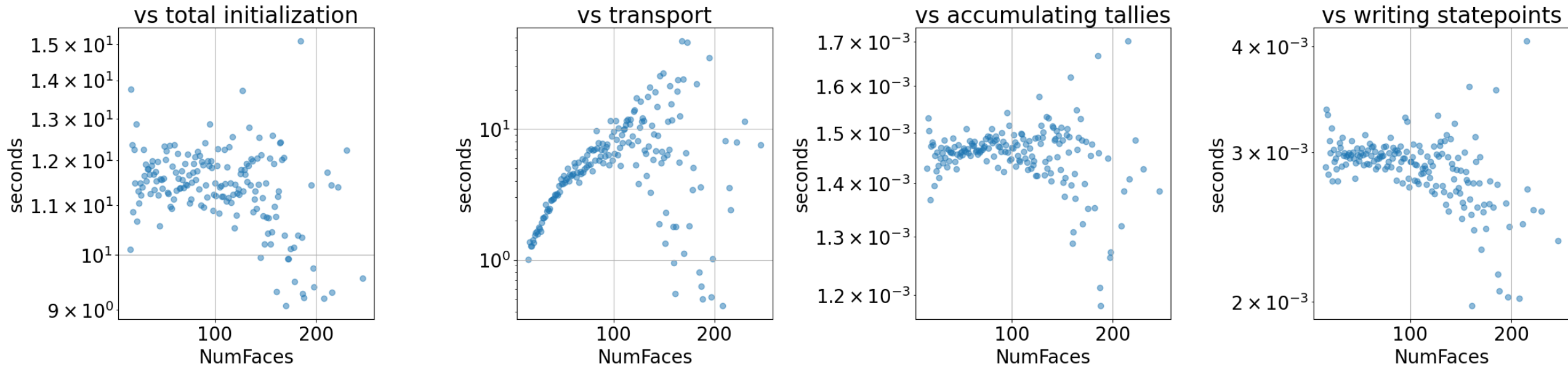
NumFaces vs..



More faces -> more runtime (but only in transport-related phase of simulation)

Results: runtime (holes)

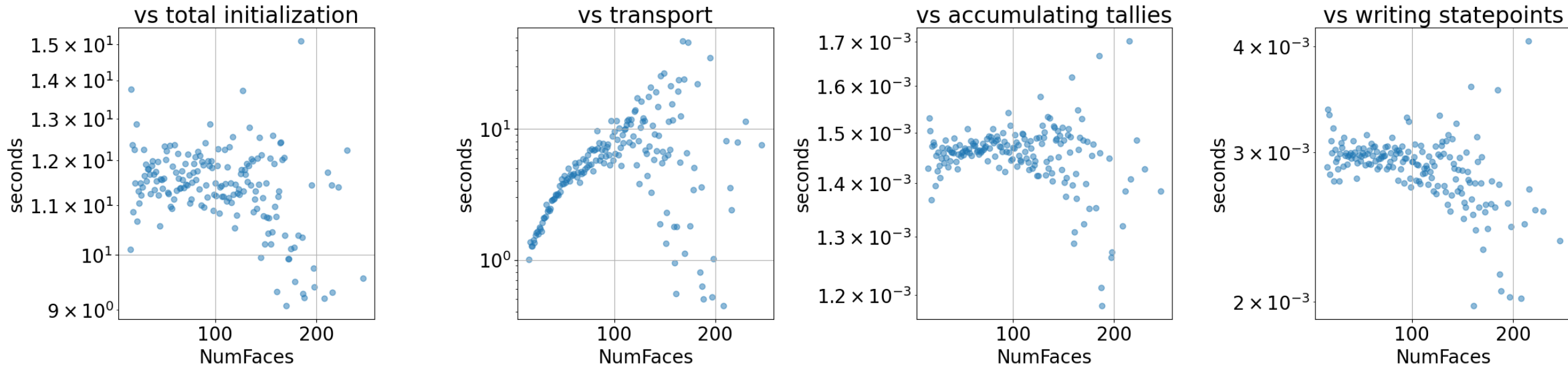
NumFaces vs..



Similar phenomenon here, but transport runtime drops at a steep gradient

Results: runtime (holes)

NumFaces vs..

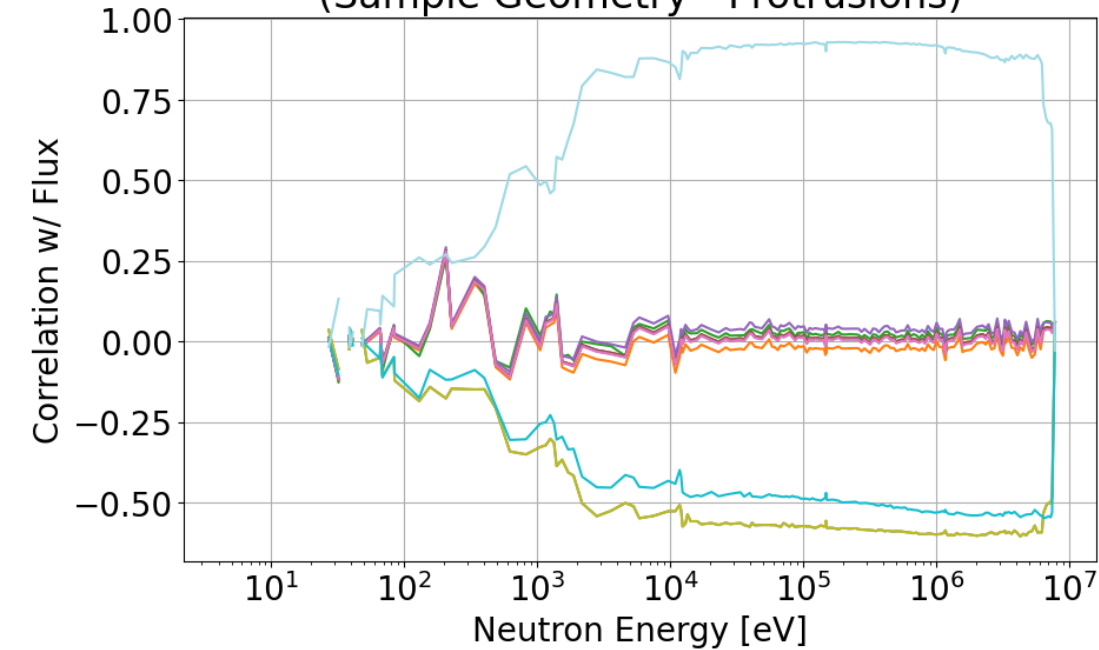


In summary, more features -> more faces -> more runtime.

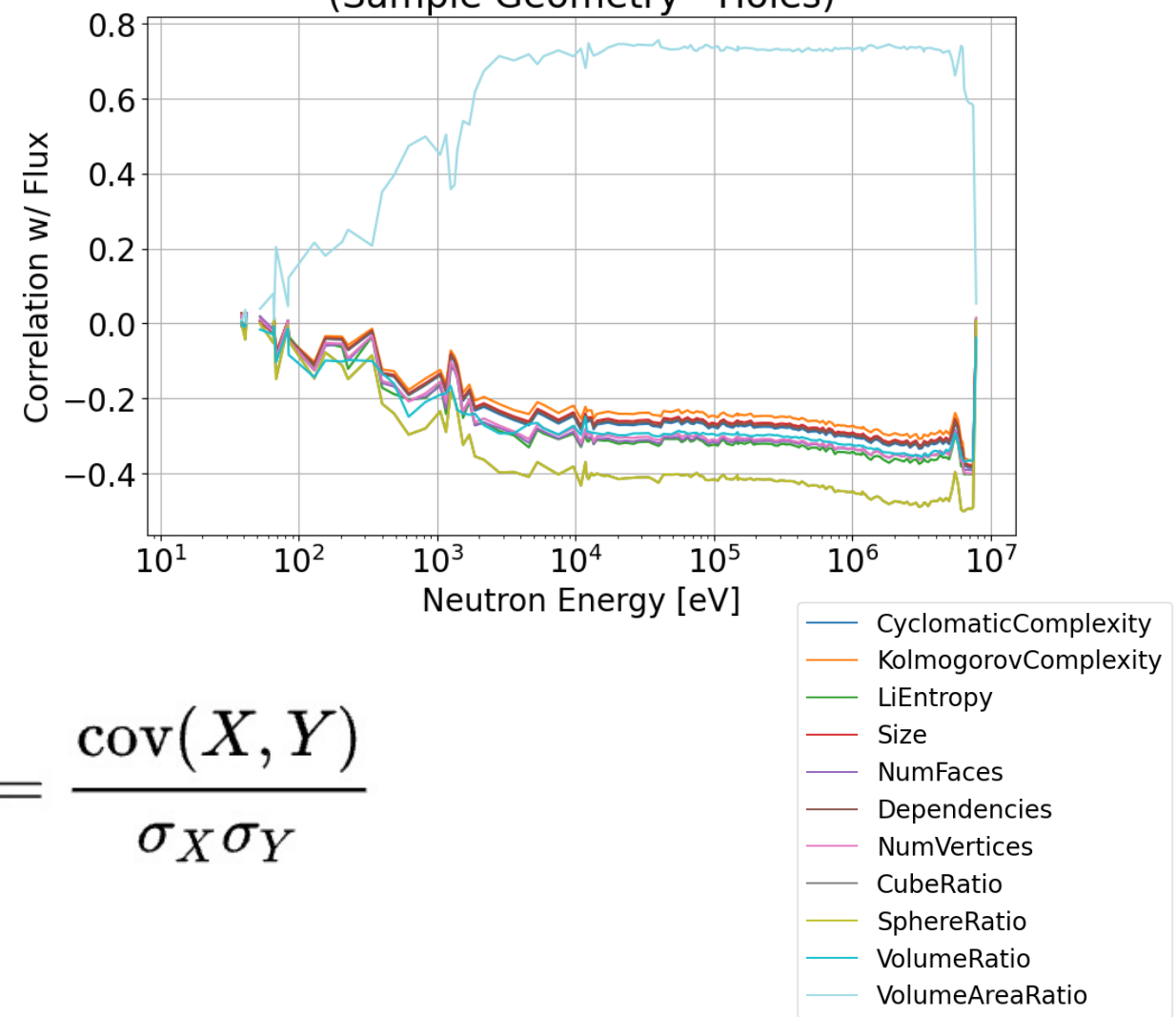
But also remember that number of faces ties in with practitioner-based complexity grading
(what CAD practitioners think a complex geometry is)

Results: flux on material sample

Correlation of Flux per Neutron Energy with Complexity Metrics
(Sample Geometry - Protrusions)



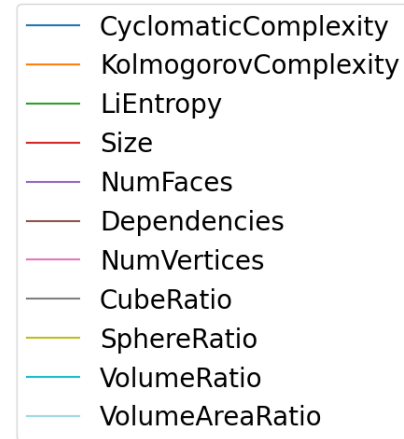
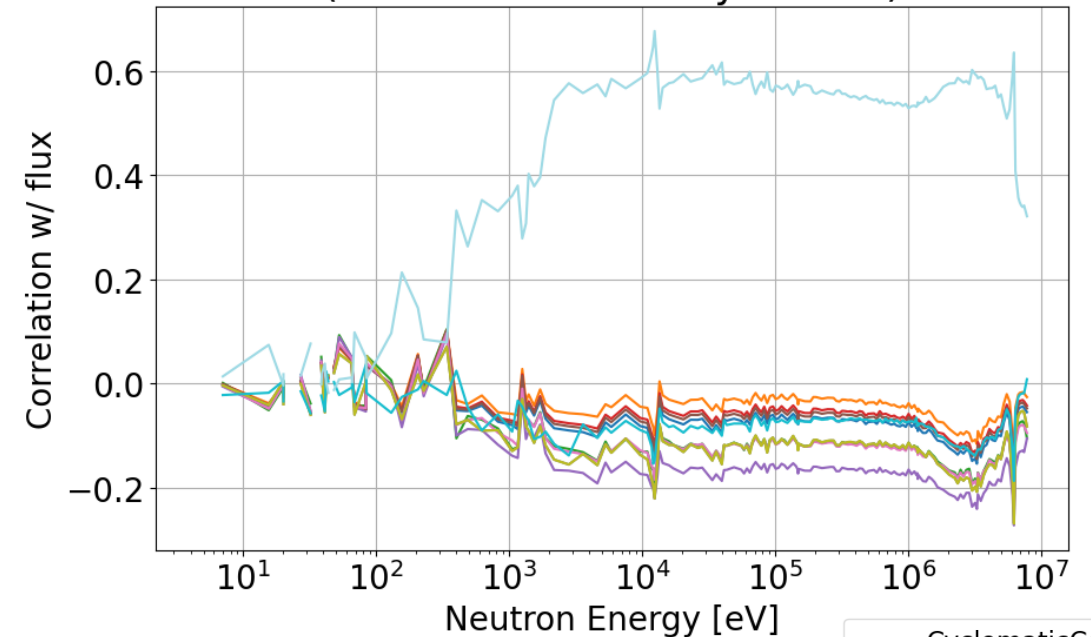
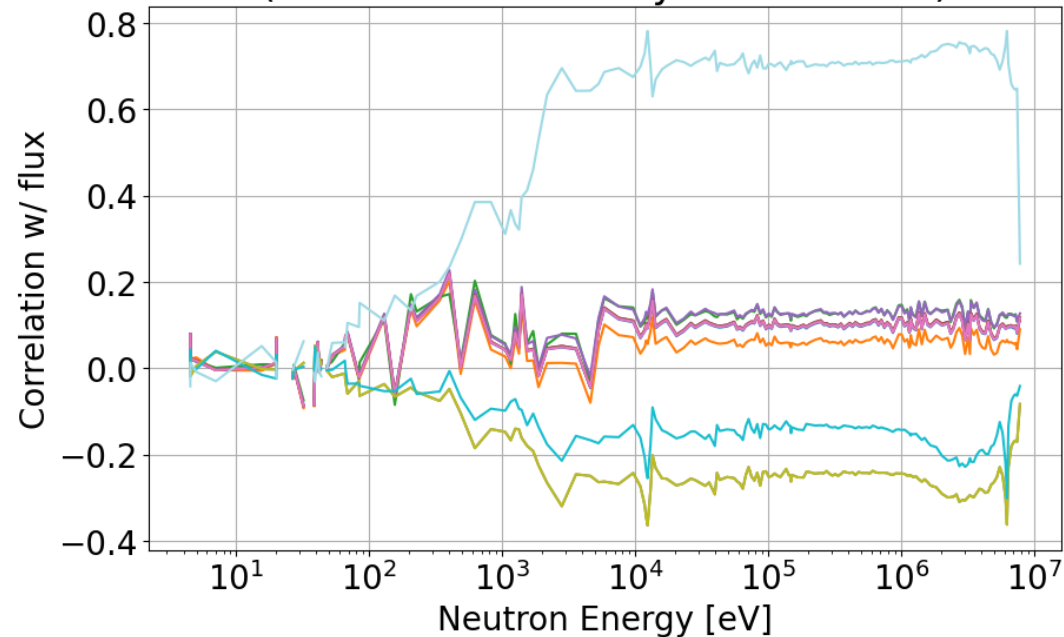
Correlation of Flux per Neutron Energy with Complexity Metrics
(Sample Geometry - Holes)



Pearson correlation coefficient:
$$\rho_{X,Y} = \frac{\text{cov}(X, Y)}{\sigma_X \sigma_Y}$$

Results: flux on enclosure

Correlation of Flux per Neutron Energy with Complexity Metrics (Enclosure Geometry - Protrusions) Correlation of Flux per Neutron Energy with Complexity Metrics (Enclosure Geometry - Holes)



- VolumeAreaRatio: Higher volume-to-surface-area ratio correlates with higher flux at higher energies.
- Cube & Sphere Ratio: Negative correlation - deviation from simple shapes may encourage less flux retention.

- What CAD practitioners think a ‘complex geometry’ is may not significantly impact actual neutronics results.
 - The strongest correlated metrics to expert-based grading do not affect neutron transport results.
 - However, **the more complex a geometry is, the longer the runtime will be** during the transport-related phase.
- Results may be influenced by overall shape compactness and deviation from simple forms like spheres and cubes

End of presentation

Thank you and questions



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trade-offs for fusion neutronics**

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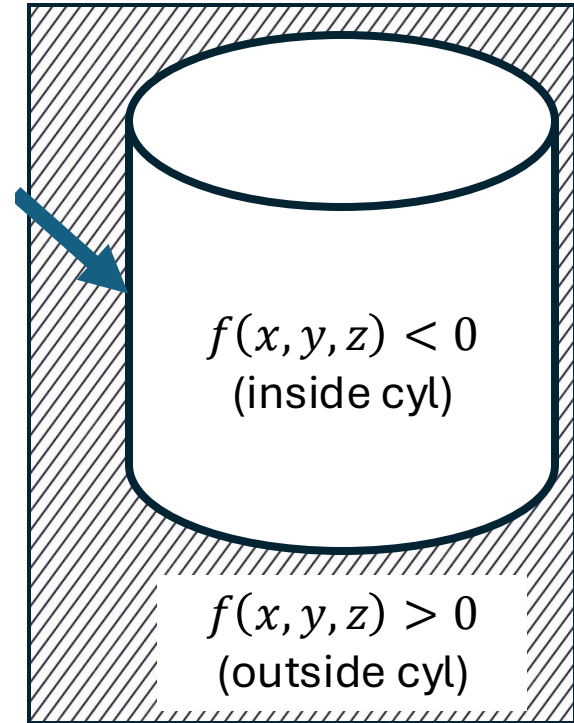
1. Contero et al. (2023), Adv. Eng. Informatics, 56, 101970
2. Collivan et al. (2022), Computer-Aided Design, 147, 103226
3. Catalan et al. (2024), Nucl. Eng. and Tech., 56(6), 2404-2411
4. Shimwell et al (2024), github.com/fusion-energy/neutronics_material_maker

- Extra slides

CSG vs DAGMC neutronics

- In **CSG**, each 'cell' is made up of regions defined in mathematical functions.
 - Cells contain material property (composition, density, temperature, etc)
- Take a cell made up of an infinite cylinder parallel to the x-axis:
$$f(x, y, z) = (y - y_0)^2 + (z - z_0)^2 - R^2 = 0$$
- We plug in:
 - Cylinder's origin for y_0 and z_0 , and radius for R
 - Particle's coordinates (x, y, z)
- If the result is less than zero, particle is inside the cylinder ('*negative half-space*')
 - Otherwise, it is outside ('*positive half-space*')
- Particles can be lost due to:
 - Cell overlaps
 - Gaps of undefined regions
- Interaction events (collision, absorption, fission) calculated based on material property of the cylinder region
- Conversion from CAD is not straightforward – many CAD geometry has splines!
 - Requires defeaturing

$f(x, y, z) = 0$
(at boundary)



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PHITS
Particle and Heavy Ion Transport code System

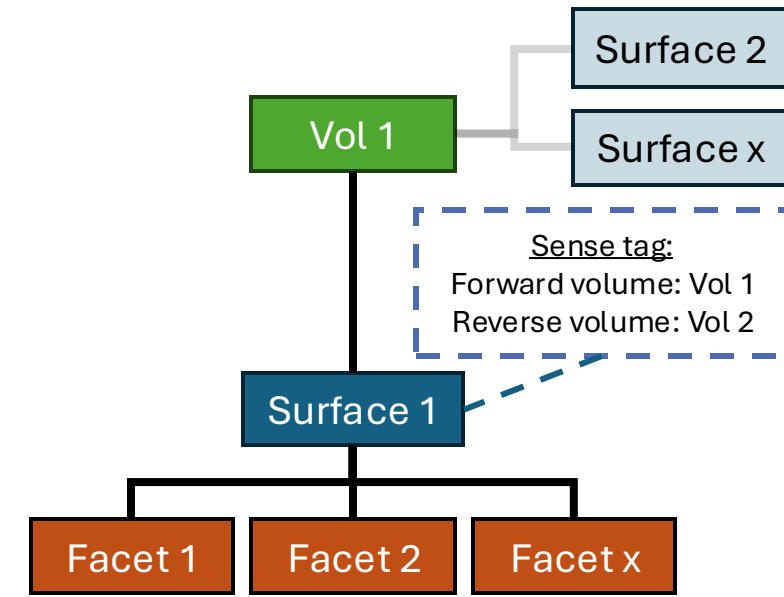


Serpent



CSG vs DAGMC neutronics

- In **DAGMC**, each 'cell' is defined by a volume bound by a surface mesh^[1]
 - Cells contain material property (composition, density, temperature, etc)
- Each mesh facet belongs to a surface, which belongs to a volume
 - Surfaces contain 'sense tags' with indicate previous & next volume
- We determine a particle's location by recording which facet it has crossed
 - From there, we can infer the surface and therefore the volume it is in
 - Has added benefit of not requiring negative space definition
- Particles can be lost due to:
 - Overlaps & undefined regions
 - Non-manifold geometry
 - Poor mesh quality
- Interaction events (collision, absorption, fission) calculated based on material property of the volume region
- Conversion from CAD relatively simple – only meshing & file conversion needed



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1. DAGMC Team (2022). Developer's Theory Guide to DAGMC. <https://svatinn.github.io/DAGMC/contribute/devtheory.html>